## University of Rhode Island [DigitalCommons@URI](https://digitalcommons.uri.edu/)

[Physical Oceanography Technical Reports](https://digitalcommons.uri.edu/physical_oceanography_techrpts) **Physical Oceanography** 

11-1988

# The SYNOP Pilot Experiment: Inverted Echo Sounder Data Report for November 1986 to March 1987

Hyun Sook Kim

Karen L. Tracey University of Rhode Island, krltracey@uri.edu

D. Randolph Watts University of Rhode Island, randywatts@uri.edu

Follow this and additional works at: [https://digitalcommons.uri.edu/physical\\_oceanography\\_techrpts](https://digitalcommons.uri.edu/physical_oceanography_techrpts?utm_source=digitalcommons.uri.edu%2Fphysical_oceanography_techrpts%2F24&utm_medium=PDF&utm_campaign=PDFCoverPages) 

#### Recommended Citation

Kim, Hyun Sook; Tracey, Karen L.; and Watts, D. Randolph, "The SYNOP Pilot Experiment: Inverted Echo Sounder Data Report for November 1986 to March 1987" (1988). Physical Oceanography Technical Reports. Paper 24.

[https://digitalcommons.uri.edu/physical\\_oceanography\\_techrpts/24](https://digitalcommons.uri.edu/physical_oceanography_techrpts/24?utm_source=digitalcommons.uri.edu%2Fphysical_oceanography_techrpts%2F24&utm_medium=PDF&utm_campaign=PDFCoverPages)

This Article is brought to you by the University of Rhode Island. It has been accepted for inclusion in Physical Oceanography Technical Reports by an authorized administrator of DigitalCommons@URI. For more information, please contact [digitalcommons-group@uri.edu](mailto:digitalcommons-group@uri.edu). For permission to reuse copyrighted content, contact the author directly.

TRACEY

# THE SYNOP PILOT

# EXPERIMENT:

Inverted Echo Sounder Data Report for November 1986 to March 1987



 $by$ Hyun Sook Kim Karen L. Tracey D. Randolph Watts

University of Rhode Island Graduate School of Oceanography Narragansett, kI 02882

GSO Technical Report Number 88-1 November 1988

ή.

## GRADUATE SCHOOL OF OCEANOGRAPHY UNIVERSITY OF RHODE ISLAND NARRAGANSETT, RHODE ISLAND

## THE SYNOP PILOT EXPERIMENT:

Inverted Echo Sounder Data Report for November 1986 to March 1987

GSO Technical Report No. 88-1

by

Hyun Sook Kim Karen L. Tracey and D. Randolph Watts

> November 1988

This research program has been sponsored by the Office of Naval Research under contract N00014-86-C-0394.

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$  $\label{eq:2.1} \mathcal{L}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}})) \leq \mathcal{L}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}})) \leq \mathcal{L}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}))$ 

 $\left\{ \right.$ 

 $\frac{1}{2}$ 

#### Abstract

The SYNOP Pilot Experiment was conducted off Cape Hatteras, from late November 1986 to early March 1987, to measure the path characteristics (position, angle, curvature), the time-varying current structure and transport of the Gulf Stream. Part of the purpose of this Experiment was to test new instrumentation techniques and moored array designs for a subsequent main SYNOP Experiment. Data collected as part of the Pilot Experiment included Inverted Echo Sounders (IESs), Current Meter moorings (CMs) and Acoustic Transport Meters (ATMs). This report documents the IES data and ATM data collected during the deployment period. Time series plots of the travel time and low-pass filtered thermocline depth measurements are presented for eleven instruments. Bottom pressure and temperature, measured at three of the sites, are also plotted. Basic statistics are given for all the data records shown. Maps of the thermocline depth field in a 160 Km by 140 Km region are presented at daily intervals.

 $\label{eq:2.1} \frac{1}{2} \int_{\mathbb{R}^3} \left| \frac{d\mu}{d\mu} \right|^2 \, d\mu = \frac{1}{2} \int_{\mathbb{R}^3} \left| \frac{d\mu}{d\mu} \right|^2 \,$  $\mathcal{L}(\mathcal{A})$  .

 $\label{eq:2.1} \mathcal{L}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}))\leq \mathcal{L}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}))\leq \mathcal{L}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}(\mathcal{L}^{\mathcal{L}}_{\mathcal{L}}))$  $\mathcal{L}_{\text{max}}$ 

 $\sim 10^{-11}$ 

 $\Delta \phi$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac$  $\frac{1}{2} \sum_{i=1}^n \frac{1}{i!} \sum_{j=1}^n \frac{1}{j!} \sum_{j=1}^n$ 

 $\label{eq:2} \frac{1}{2} \int_{0}^{2\pi} \frac{1}{2} \, \mathrm{d} \phi \, \mathrm{d} \phi \, \mathrm{d} \phi \, \mathrm{d} \phi$ 

 $\mathcal{F}_{\mathcal{G}}$  ,



 $\frac{1}{2}$ 

 $\frac{1}{2}$ 

 $\boldsymbol{\beta}$ 



 $\frac{1}{2}$ 

 $\mathbf{v}$ 

 $\bar{\star}$ 

i,

# List of Figures





 $\hat{\mathcal{E}}$  $\frac{1}{2}$ 

į

## List of Tables



 $\ddot{\bullet}$ 

vii

 $\blacksquare$ 

#### **Experiment Description and Data processing**  $\mathbf{1}$

#### $1.1$ Introduction

This report documents data collected using Inverted Echo Sounders (IESs) in the Gulf Stream off Cape Hatteras from November 1986 to March 1987. The measurements were made under the support of an ONR project entitled "SYNOP Pilot Experiment." Other data collected as part of this Pilot Experiment included (a) two Current Meter moorings (CMs) with five levels of each mooring, at depths of 400, 700, 1000 and 2000 m and 50 m above the bottom (Co-P.I., J. Bane, University of North Carolina), (b) tests of two acoustic doppler current profilers at the top of these moorings (W. Johns, University of Miami), (c) tests of two Acoustic Transport Meters (ATMs) (D.R. Watts, University of Rhode Island), (d) Pegasus surveys of velocity and temperature sections (K. Leaman, University of Miami), (e) tests of a new electromagnetic towed transport meter (T. Sanford, University of Washington, APL), and (f) Pop-up-profiler (A. Bradley, WHOI). The ATM data are included in this report. The other data will be documented separately.

The principal objectives of the IES and ATM portion of this SYNOP Pilot Experiment are as follows:

- 1. developing improved techniques for monitoring inflow conditions of the Gulf Stream as it leaves Cape Hatteras, and
- 2. mapping the thermocline topography by objective analysis in the region surrounding the current meter and Pegasus surveys.
- The specific inflow conditions that we wish to monitor are
- path characteristics (position, angle, curvature)
- detailed cross-stream structure of the thermocline
- baroclinic and barotropic transport
- $-$  stream function and vorticity.

To contribute to our planned dynamical and statistical studies later in the SYNoptic Ocean Prediction program (SYNOP), these inlet parameters are seen as a generalization

 $\mathbf 1$ 

and improvement of earlier work for the purpose of specifying "inlet conditions" for numerical prediction of the synoptic variability of the Gulf Stream farther downstream.

To address these objectives, an array of IESs, CMs and ATMs were deployed within the Gulf Stream near 35°N 74°W. In this region, there is a minimum in the lateral meander motion, as determined from several years of satellite observations of the Gulf Stream's surface temperature front.

The nine IESs and two ATMs (and two CMs) were deployed on a cruise aboard the R/V ENDEAVOR (EN152) from 20 November to 3 December 1986, and recovered on the  $R/V$ ENDEAVOR (EN156) from 26 February to 6 March 1987. During this three-month-period, the instruments were located on three sections in an rectangular grid 160 Km downstream by 140 Km cross-stream. The IES sites, designated by the solid circles in Figure 1, are spaced 35 Km cross-stream and 50 Km alongstream. Acoustic transport meters and current meter moorings are located at the sites shown by the two solid triangles. These are situated halfway between adjacent IESs, thereby giving a 35 Km spacing between them as well. Additionally, bottom pressure gauges and bottom temperature sensors are included at three IES sites located along line B (indicated by the solid box). All IES and ATM sites are listed in Table 1.

#### **Site Naming Conventions** 1.2

The three cross-stream sections are designated from west to east by the letters A through C. The IES sites along line A and line C are numbered from 1 through 2, and line B consecutively from 1 through 7, with site 1 located at the northwestern end of the section. In this report, each instrument site is referred to by both the section letter and site number, prefaced by either IES, if it is a standard instrument, or PIES, if it is a combined IES and bottom pressure gauge. For example, IES87B5 is the fifth site from the northern end of line B. Additionally, the preface ATM indicates an acoustic transport meter site.



# Figure 1: The SYNOP Pilot Experiment field observations area.

All IES (circles) and ATM (triangles) sites were occupied from November 1986 through February 1987. PIESs with bottom pressure gauges and temperature sensors are located at the solid rectangluar boxes. The box is the 160 Km by 140 Km region, which is shown in Figure 12. The solid line through the area shows the historical mean path of the Gulf Stream.



#### DEPLOYMENT DURIOR IN LEBOX

#### 1.3 **Inverted Echo Sounder Description**

A detailed description of the IES is presented in Chaplin and Watts (1984) and will not be repeated here. Briefly, however, the IES is an instrument which is moored one meter above the ocean floor and which monitors the depth of the main thermocline acoustically. A sample burst of acoustic pulses is transmitted every half hour and round trip travel times to the surface and back are recorded on a digital cassette tape within the instrument. For the standard IES, a sample burst typically consists of twenty 10 KHz pings. Additionally, bottom pressure and temperature can be measured and recorded. For instruments with these optional sensors, the travel time burst consists of 24 pings, whereas the pressure and temperature are average measurements over the whole sampling interval.

#### 1.4 Data Processing

Most of the earlier processing was done on a PRIME 750 computer, except for the initial dumping of the data from the cassette tapes onto a 9-track magnetic tape. This was done on the Hewlett Packard 2000 series computer maintained by the URI Marine Technicians. At the last major step, objective mapping, the processing was done on our Micro Vax II computer system. The basic processing steps, which include transcription, editing, and conversion into scientific units, are illustrated by the flowchart in Figure 2. The data processing is accomplished by a series of routines specifically developed for the IES. Since these programs are documented elsewhere (Tracey and Watts, 1988), the steps are only outlined below.

- RAW DATA CASSETTES : Recorded within the instruments. Contain the counts associated with travel time, pressure, and temperature measurements as a series of integer words of varying lengths.
- CARP : Transfers the data from cassettes to 9-track magnetic tape for subsequent processing.
- BUNS : Converts the series of integer words of varying lengths into standard length 32-bit integer words.
- PUNS : Produces integer listings and histograms of the travel time sample bursts. Provides an initial look at data quality and travel time distributions. Used to determine the first (after launch) and last (before recovery) 'on bottom' samples.
- MEMOD : Establishes the time base. Determines either the median or modal value (at the user's option) of the travel time burst as the representative measurement. Converts all travel time, pressure and temperature counts into specific units of seconds, decibars, and degrees Celsius, respectively.
- FILL : Checks for proper incrementing of the time base. Missing data points are filled by inserting interpolated values.
- DETIDE : From user-supplied tidal constituents specific to each site, determines the tidal contribution to the travel times and removes it from the measured values.

Instrument Cassette<br>Data Tape  $CARP$ (9-TRACK)<br>DATA<br>TAPE **PUNS BUNS**  $\bar{1}$ MEMOD FILL DETIDE DESPIKE PLOT SEACOR PLOT Low-pass<br>Filtering PLOT Objective<br>Mapping



**DESPIKE**: Identifies and replaces travel time spikes with interpolated values.

- SEACOR: Removes the effects of seasonal warming and cooling of the surface layers from the travel times. Plots of the half-hourly pressure, temperature and travel time are generated.
- LOW PASS FILTERING : Convolves the travel times, pressures, and temperatures with a 40 hours low-pass Lanczos filter. The smoothed series are subsampled at six hour intervals and plotted.
- **OBJECTIVE MAPPING** : Produces daily maps of the depth of the 12°C isotherm as documented in Watts, Tracey and Friedlander, 1988.

The FESTSA time series analysis package (Brooks, 1976), modified for the PRIME 750, was used to remove the higher frequency (tidal and inertial) motions from those with periods of several days or longer, which are the main focus of this project. The symmetric filter, with a Lanczos taper, was designed with the quarter power point at 0.025 cph and the tidal cycle attenuated by 60 dB. The half-hourly travel time, pressure, and temperature data were low-pass filtered and the smoothed output series (40 HRLP) had sampling intervals of six hours.

#### **Travel Time Calibration** 1.4.1

Variations in the travel times have been shown to be proportional to variations in the thermocline depth (Watts and Rossby, 1977; Watts and Wimbush, 1981). Calibration XBTs were taken at each IES site in order to convert the travel times  $(\tau)$  into thermocline depths ( $\xi$ ) according to the relation:  $\xi = M\tau + B$ , where M is a scale factor and the intercept B depends on the depth of the instrument. Regressions of  $\tau$  versus  $\xi$ , performed for several instruments, show that the constant (M) value,  $M = -19.0$  m/msec for the 12°C isotherm, is appropriate for all these Gulf Stream sites. The values of B used for each instrument are listed in the tables in Section 2. For practical purposes the main thermocline depth can be represented by the depth of an individual isotherm. For this work, we have chosen the 12°C isotherm since it is situated near the highest temperature gradients of the main thermocline and correlates well with  $\tau$  (Rossby, 1969; Watts and Johns, 1982). The low-pass

filtered travel time records were scaled to the thermocline depths  $(Z_{12})$  and these records are shown in Section 4. Since  $\tau$  is resolved to 0.1 msec, the 40 HRLP  $Z_{12}$  scaled values are therefore resolved to  $\pm 2$  m. However, the accuracy of the offset parameter B is estimated to be  $\pm 25$  m for most instruments, judged from the agreement between the several calibration XBTs taken at each site. Relative to this, the 40 HRLP  $Z_{12}$  values are resolved to  $\pm 2$  m.

#### 1.4.2 Thermocline Depth Mapping

Objective maps of the thermocline  $(Z_{12})$  field in the array region have been produced at daily intervals from these records. The boxed region in Figure 1, oriented 045°T, is the region which has been mapped. The objective mapping techniques were developed by E. Carter (1983) and special adaptations for their application to the Gulf Stream frontal zone are discussed in Watts and Tracey (1985). Two results presented in this latter work are of particular importance to the objective mapping performed here: 1) If the mean field is removed, the perturbations have essentially isotropic correlation fields. 2) The space-time correlation functions used for the objective analysis are shown.

The objective analysis is performed on the "perturbation fields", which are obtained by removing the mean field from the input dataset and normalizing by the standard deviation. To represent the mean field,  $\overline{Z_{12}}(x,y)$ , where x is alongstream (045°T) and y is crossstream (315°T), a third order polynomial was fitted to the mean values observed during the November 1986 to March 1987 deployment period. The function form of the polynomial was:

$$
\overline{Z_{12}}(x,y) = B_0 + B_1x + B_2y + B_{11}x^2 + B_{12}xy + B_{22}y^2 + B_{111}x^3 + B_{112}x^2y + B_{122}xy^2 + B_{222}y^3
$$

where  $(x,y)$  is the position in kilometers from the origin at 35°N, 74°W,  $B_o$  is 0.76533772 $E+$ 03,  $B_1$  is 0.6320926E + 00,  $B_2$  is -0.4103623E + 01,  $B_{11}$  is -0.8553885E - 02,  $B_{12}$  is  $0.1851212E - 01, B_{22}$  is  $-0.5083383E - 01, B_{111}$  is  $0.5500527E - 04, B_{112}$  is  $-0.9935370E -$ 04,  $B_{122}$  is  $-0.6128939E - 04$ , and  $B_{222}$  is 0.3236166E - 03. The standard deviation field,  $\sigma(x, y)$ , was defined as a function of the mean field depth, from a Gaussian form representative of all IES records:

$$
\sigma(x,y) = A + Bexp\left(-\left[\frac{\overline{Z_{12}}(x,y) - Z_o}{C}\right]^2\right)
$$

where A is 50 m, B is (200 m - A), C is 200 m,  $Z_0$  is 470 m, and  $\overline{Z_{12}}(x, y)$  is the mean thermocline depth at that (x,y) location. Figure 10 shows both the mean and standard deviation fields in plain view. The objectively estimated error fields are shown in Figure 11.

For each output grid point, the objective mapping technique selects, from all the input data within a specified maximum time lag  $(T)$  and radial  $(R)$ , the number of the points  $(N)$ which have the highest correlations. The output fields in Figure 12 result from specifying  $N = 6$ ,  $T = \pm 1$  days,  $R = 120$  Km, and using the idealized correlation function (Watts and Tracey, 1985) with an assumed noise level  $E = 0.05$ .

The output of the objective mapping is the perturbation field on a full grid of points, with 20 Km grid spacing, within a 160 Km by 140 Km mapping region. The thermocline depth maps (shown in Figure 12) are obtained by renormalizing the perturbation field by the standard deviation and restoring the mean. Tracey et al. (1987) report an accuracy of 47 m for these output  $Z_{12}$  fields.

#### 1.4.3 Temperature

Temperatures (Figure 6) were measured using thermistors (Yellow Springs International Corp., model 44032) controlled by Sea Data Corp. (model DC-37B) electronics cards installed in the IESs, in order to correct the pressure values for the temperature sensitivity of the transducer. The thermistor is inside the instrument, on the pressure transducer, rather than in the water. However, once the temperature probe has reached equilibrium with the surrounding waters, it also provides accurate measurements of the bottom temperature fluctuations (effectively low-pass filtered with a 40 hour e-folding equilibrium time). The first 24 half-hourly points were dropped prior to low-pass filtering, since the temperatures took 12 hours to reach equilibrium within 0.001°C. The accuracy of the temperature measurements is about 0.1°C, and the resolution is 0.0002°C.

#### 1.4.4 **Bottom Pressure**

Digiquartz pressure sensor (models 46K-032 and 76KB-032) manufactured by Paroscientific, Inc. were used to measure bottom pressure. All pressure measurements were corrected for the temperature sensitivity of the transducer, using calibration coefficients purchased from the manufacturer. The half-hourly measured bottom pressures (Figure 4) are dominated by the tides, however for some of the instruments, the pressures also drift, 0(0.4 dbar), monotonically with time. Processing of the pressure measurements includes removing the long-term drift and tides as follows.

Tidal response analysis (Munk and Cartwright, 1977) was used to determine the tidal constituents for each instrument. The calculated tides were then removed from the pressure records. The amplitudes, H (dbar), and phases,  $G^{\circ}$  (Greenwich epoch), of the constituents are given in the tables in Section 2.

In order to estimate and remove the long-term drift from the measurements, we made least-squares fits of exponential and exponential-linear curves to our data (Watts and Kontoyiannis, 1986). The mathematical formulas we used here were:

$$
Drift = P_1[1 - exp(P_2t)] + P_3
$$

for the exponential curve and

$$
Drift = P_1[1 - exp(P_2t)] + P_3 + P_4t
$$

for the exponential-linear curve. Here t is the time in hours, relative to the approximate deployment time, which is 13 hours before the first data point used.  $P_1$ ,  $P_2$ ,  $P_3$ , and  $P_4$ are free parameters determined for each instrument by the non-linear regression subroutine P3R of BMDP-79, a package of computer programs developed at the Health Science Computing Facility, UCLA (Dixon and Brown, 1979). These coefficients are listed in Section 2 for PIES87B1 and PIES87B3.

The half-hourly pressures are resolved to 0.001 dbar and the mean pressure is accurate to within 1.5 dbar. We estimate that the residual (drift and tide removed) bottom pressure records, shown in Figure 5, have an accuracy (relative to their mean pressure) of better than 0.05 dbar (Watts and Kontoyiannis, 1986). The residual bottom pressure records were low-pass filtered (Figure 8) as mentioned above.

#### 1.4.5 **Time Base**

The date and time were assigned to each sampling period. The tables in Section 2, report the hours, minutes, and seconds associated with the first and last sampling period as a six-digit number. All times are given as Greenwich Mean Time (GMT). For processing convenience, the times were converted into yearhours. Table 2 lists the yearhour which corresponds to 0000 GMT of each day for non-leap years. (For leap years, the yearhours can be determined by adding 24 to each day after February 28.) There are a total of 8760 hours in a standard year and 8784 hours in a leap year. The yearhours given in this report are referenced to January 1, 1987 at 0000 GMT, with measurements occurring between January and March 1987 assigned positive yearhours. Negative values correspond to the sampling period from November through December 1986.

#### $1.5$ **Acoustic Ocean-Transport Meter Description**

The acoustic transport meter, described in Chaplin and Watts (1986), is a new instrument which is presently under development. We conducted the first extensive test deployments of the ATM prototypes during the SYNOP Pilot Experiment.

The ATM consists of three separate components, a master transceiver and two slave transponders. These components are moored in a triangular pattern, at nominal spacings of 3 Km. The master is a microprocessor-controlled IES which has had its sampling scheme reprogrammed. The typical configuration has 32 measurements taken per hour at approximately 56 s intervals to allow ample time for all signals to be received and/or dissipated.

In addition to measuring transport, the master and slave components can perform other operations. The master functions as a traditional IES, measuring the thermocline depth at its deployment site. The two slaves can serve as navigation transponders for the Pegasus velocity profiler. During a Pegasus drop, the ATM is sent a coded signal and sampling is reduced to one measurement per hour so as not to interfere with the Pegasus acoustics.



 $\sim$ 

 $\mathcal{A}$ 



 $\bar{z}$ 

 $\sim$ 

 $12\,$ 

 $\ddot{\phantom{a}}$ 

 $\sim 10^7$ 

 $\ddot{\phantom{0}}$ 

 $\bar{z}$ 

After the Pegasus operations have been completed, normal sampling resumes.

Unfortunately during the Pilot Experiment, the ATMs did not function correctly. Two unrelated problems occurred which resulted in poor data returns. First, deploying the three ATM components at just the right spacings so that all the required acoustic signals are received without interfering with each other or with extraneous echos is a more subtle and difficult job than we had realized. Consequently, the deployment sites of the three ATM components were not optimal, and some of the acoustic signals required for the transport calculations either were not recorded or interfered with each other's detected transit time. Hence, in this report only thermocline depth measurements are reported for the ATMs.

Secondly, after operating normally for several days, both instruments automatically switched from the "normal" sampling mode into the "Pegasus" sampling mode. For one instrument, ATM87B2, even the Pegasus-mode was unusual with 8 measurements made at irregular intervals during each hour. Thus special data processing was required to obtain accurate thermocline depth values from the travel time measurements.

The data records of both ATM87B2 and ATM87B4 were split into two sections based on the sampling modes. Different processing was performed on the different sections.

Both instruments sampled normally (32 measurements per hour) during the first portions. These travel time data were grouped into hourly "bursts" and processed as in Section 1.4 for an IES through the MEMOD and DESPIKE programs. Since these initial records were only about five days long, the high frequency motions were removed using a 12-hour lowpass-filter in place of the typical 40-hour lowpass-filter. The output data were subsampled at 6-hour intervals and scaled to thermocline depths. Since these records are very short, they are not shown in Figures 3.2 and 7.2. However the data have been used to contribute to the objective maps shown in Section 5.

For the two instruments, the second portions (Pegasus-mode) of the travel time records were processed differently. For ATM87B2, with only 8 samples per hour, the data were grouped into 12-hour "bursts" prior to IES processing and removing the travel time spikes. The data for ATM87B4, with only one sample per hour, were similarly grouped and processed, except in 24-hour "bursts". For both instruments, the start time for each "burst" is stepped forward at a 6 hour interval (the bursts overlap). The processed vertical travel time data from the ATMs are shown in Figure 3.2. Lowpass-filtering was performed using a 96-hour Lanczos filter. The filtered data (Figure 7.2) have a sampling interval of 24 hours and were scaled to thermocline depths in the same manner as for the other IESs.

#### 1.6 Data Recovery

Table 1 summarizes the data returns from each of the IESs and ATMs. All nine instruments were recovered, giving a recovery rate of 100%. IES87C1 ceased functioning properly about one month after the instrument was launched. All the remaining instruments performed successfully, yielding a 91% data return for the travel time measurements. Complete records were obtained from all three bottom pressure gauges; however the data record from one of these (PIES87B6) had large jumps, indicating its sensor malfunctioned, thus the recovery rate for the bottom pressure data was only 67%. Complete records were obtained from all three temperature gauges; thus the return rate was 100% for these data.

#### Individual Site and Record Information Tables  $\overline{2}$

The following tables provide informations about the location, dates, and basic statistics on the data records. Each table documents a single instrument site.

General site information, such as position, bottom depth, and launch and recovery times, is given first. Subsequently, details about the travel time, bottom pressure, temperature and thermocline depth records plotted in Section 3 and 4 are tabulated. For each plot, the times associated with the first and last data point are supplied. All yearhours are referenced to January 1, 1987 at 0000 GMT. Measurements made during the calendar year prior to the reference date are given as negative yearhours.

The first order statistics (minimum, maximum, mean, and standard deviation) were calculated for the half-hourly and 40 HRLP records for each variable of standard IES and PIES, and for the six-hourly and 96 HRLP records for that of two ATMs. These are also presented in the following tables.

## Table 3. Site and Record Information for **IES87A1**

Serial Number: 043 Type of Travel Time Detector: TTC Number of Pings per Sampling: 20 Additional Sensors: None

POSITION: 35°16.12 N DEPTH: 2660 m 74°32.94 W



#### TRAVEL TIME RECORDS Fig. 3.1



Number of Points: 4544 Sampling Interval: 0.5 hrs



#### 40HRLP THERMOCLINE DEPTH RECORDS Fig. 7.1

 $Z_{12}$  Conversion equation:  $Z_{12} = -19000 \text{ms}^{-1} \cdot \tau_d + B$ where  $B = 67541.63 m$ Travel Time (sec) with tide removed  $\tau_d =$ 



Number of Points: 369 Sampling Interval: 6.0 hrs

Minimum  $Z_{12} = 313.34$  m Mean =  $447.74 \text{ m}$ Maximum  $Z_{12} = 522.71 \text{ m}$  Standard Deviation = 46.97 m

#### Table 4. Site and Record Information for **IES87A2**

Serial Number: 045 Type of Travel Time Detector: TTC Number of Pings per Sampling: 20 Additional Sensors: None

POSITION: 34°58.08 N DEPTH: 3280 m 74°07.89 W



#### TRAVEL TIME RECORDS Fig. 3.1



Number of Points: 4542 Sampling Interval: 0.5 hrs



#### 40HRLP THERMOCLINE DEPTH RECORDS Fig. 7.1

 $Z_{12}$  Conversion equation:  $Z_{12} = -19000 \text{ms}^{-1} \cdot \tau_d + B$ where  $B = 83377.92 m$  $\tau_d =$  Travel Time (sec) with tide removed



Number of Points: 369 Sampling Interval: 6.0 hrs



### Table 5. Site and Record Information for PIES87B1

Serial Number: 058 Type of Travel Time Detector: TTC Number of Pings per Sampling: 24 Additional Sensors: Pressure and Temperature Pressure Sensor Serial Number: 19327

#### POSITION: 35°45.64 N DEPTH: 1950 m 74°27.93 W



#### TRAVEL TIME RECORDS Fig. 3.2



#### Number of Points: 4537 Sampling Interval: 0.5 hrs

Minimum  $\tau = 0.19395$  s  $Mean = 0.20100 s$ Maximum  $\tau = 0.20586$  s Standard Deviation = 0.00193 s

#### 40HRLP THERMOCLINE DEPTH RECORDS Fig. 7.2

 $Z_{12}$  Conversion equation:  $Z_{12} = -19000 \text{ms}^{-1} \cdot \tau_d + B$ where  $B =$ 4045.00 m Travel Time (sec) with tide removed  $\tau_d =$ 



Number of Points: 368 Sampling Interval: 6.0 hrs

Minimum  $Z_{12} = 164.37$  m  $Mean = 226.57 m$ Maximum  $Z_{12} = 313.92$  m Standard Deviation = 33.06 m

#### PIES87B1 (continue)

### MEASURED PRESSURE RECORDS Fig.  $4$



Number of Points: 4537 Sampling Interval: 0.5 hrs

Minimum  $= 1964.16$  dbar  $Mean = 1964.88$  dbar Maximum = 1965.79 dbar Standard Deviation =  $0.33140$  dbar

#### RESIDUAL PRESSURE RECORDS Fig.  $5$

 $P_{residual} = P_{measured} - MEAN - DRIFT - TIDE$ DRIFT =  $P_1[1 - exp(P_2t)] + P_3 + P_4t$ where  $t =$  Time of sample in hours, starting with  $t = 13.0$  hrs for the first data point  $P_1 =$ 1.167470 dbar  $P_2 = -0.000321$  dbar  $P_3 =$ 0.078548 dbar  $P_4=$ 0.000231 dbar

TIDE calculated from the following constituents:



Number of Points: 4513 Sampling Interval: 0.5 hrs



19

## PIES87B1 (continue)

#### **40HRLP PRESSURE RECORDS** Fig.  $8$



Number of Points: 366 Sampling Interval: 6.0 hrs



#### TEMPERATURE RECORDS Fig.  $6$



Number of Points: 4537 Sampling Interval: 0.5 hrs

Minimum  $= 3.490 °C$ Mean =  $3.784$  °C Maximum = 3.991 °C Standard Deviation =  $0.103$  °C

#### 40HRLP TEMPERATURE RECORDS Fig. 9



Number of Points: 366 Sampling Interval: 6.0 hrs



## Table 6. Site and Record Information for **ATM87B2**

Serial Number: 064 Type of Travel Time Detector: TTD Number of Pings per Sampling: refer to Sec. 1.5 Additional Sensors: None

POSITION: 35°40.67 N DEPTH: 2300 m 74°23.52 W



### RAW TRAVEL TIME RECORDS Fig. 3.2



Number of Points: 343 Sampling Interval: 6.0 hrs



#### 96HRLP THERMOCLINE DEPTH RECORDS Fig. 7.2

 $Z_{12}$  Conversion equation:  $Z_{12} = -19000 \text{ms}^{-1} \cdot \tau_d + B$ where  $B = 57875.36$  m  $\tau_d =$  Travel Time (sec) with tide removed



Number of Points: 81 Sampling Interval: 24 hrs



### Table 7. Site and Record Information for **PIES87B3**

Serial Number: 053 Type of Travel Time Detector: TTC Number of Pings per Sampling: 24 Additional Sensors: Pressure and Temperature Pressure Sensor Serial Number: 17849

#### POSITION: 35°37.07 N DEPTH: 2665 m 74°13.92 W



#### TRAVEL TIME RECORDS Fig. 3.2



Number of Points: 4532 Sampling Interval: 0.5 hrs



#### 40HRLP THERMOCLINE DEPTH RECORDS Fig. 7.2

 $Z_{12}$  Conversion equation:  $Z_{12} = -19000 \text{ms}^{-1} \cdot \tau_d + B$ where  $B = 7224.39 \text{ m}$  $\tau_d =$  Travel Time (sec) with tide removed



Number of Points: 368 Sampling Interval: 6.0 hrs



#### PIES87B3 (continue)

#### MEASURED PRESSURE RECORDS Fig.  $4$



Number of Points: 4532 Sampling Interval: 0.5 hrs

Minimum  $= 2707.75$  dbar  $Mean = 2708.47$  dbar Maximum = 2709.34 dbar Standard Deviation =  $0.33335$  dbar

#### RESIDUAL PRESSURE RECORDS Fig. 5

 $P_{residual} = P_{measured} - MEAN - DRIFT - TIDE$ DRIFT =  $P_1[1 - exp(P_2t)] + P_3$ where  $t =$  Time of sample in hours, starting with  $t = 13.0$  hrs for the first data point  $P_1 = 0.8711981$  dbar  $P_2 = 0.0000230$  dbar  $P_3 = 0.0237850$  dbar

TIDE calculated from the following constituents:





Number of Points: 4508 Sampling Interval: 0.5 hrs



## PIES87B3 (continue)

### **40HRLP PRESSURE RECORDS** Fig. 8



Number of Points: 366 Sampling Interval: 6.0 hrs



### TEMPERATURE RECORDS Fig.  $6$



Number of Points: 4532 Sampling Interval: 0.5 hrs

Minimum =  $2.570 °C$ Mean =  $2.837$  °C Maximum =  $3.088 °C$  Standard Deviation =  $0.124 °C$ 

 $\ddot{\phantom{a}}$ 

### 40HRLP TEMPERATURE RECORDS Fig. 9



Number of Points: 366 Sampling Interval: 6.0 hrs



## Table 8. Site and Record Information for **ATM87B4**

Serial Number: 063 Type of Travel Time Detector: TTD Number of Pings per Sampling: refer to Sec. 1.5 Additional Sensors: None

### POSITION: 35°26.50 N DEPTH: 3085 m  $73^{\rm o}59.47~{\rm W}$



#### RAW TRAVEL TIME RECORDS Fig. 3.2



Number of Points: 332 Sampling Interval: 6.0 hrs

Minimum  $\tau = 4.07544$  s  $Mean = 4.07870 s$ Maximum  $\tau = 4.08579$  s Standard Deviation = 0.01749 s

### 96HRLP THERMOCLINE DEPTH RECORDS Fig. 7.2

 $Z_{12}$  Conversion equation:  $Z_{12} = -19000 \text{ms}^{-1} \cdot \tau_d + B$ where  $B = 78181.09 \text{ m}$  $\tau_d =$  Travel Time (sec) with tide removed



Number of Points: 79 Sampling Interval: 24 hrs



### Table 9. Site and Record Information for **IES87B5**

Serial Number: 052 Type of Travel Time Detector: TTC Number of Pings per Sampling: 20 Additional Sensors: None

**POSITION: 35°22.06 N** DEPTH: 3280 m 73°53.06 W



#### TRAVEL TIME RECORDS Fig. 3.2



Number of Points: 4509 Sampling Interval: 0.5 hrs

Minimum  $\tau = 4.36937$  s Mean =  $4.37362 s$ Maximum  $\tau = 4.37918$  s Standard Deviation = 0.00130 s

#### 40HRLP THERMOCLINE DEPTH RECORDS Fig. 7.2

 $Z_{12}$  Conversion equation:  $Z_{12} = -19000 \text{ms}^{-1} \cdot \tau_d + B$ where  $B = 83818.94 \text{ m}$  $\tau_d =$  Travel Time (sec) with tide removed



Number of Points: 366 Sampling Interval: 6.0 hrs

Minimum  $Z_{12} = 641.63$  m  $Mean = 719.65 m$ Maximum  $Z_{12} = 775.03$  m Standard Deviation = 21.17 m
## Table 10. Site and Record Information for PIES87B6

Serial Number: 054 Type of Travel Time Detector: TTC Number of Pings per Sampling: 24 Additional Sensors: Pressure and Temperature Pressure Sensor Serial Number: 18426

### POSITION: 35°14.54 N DEPTH: 3555 m 73°42.92 W



### TRAVEL TIME RECORDS Fig. 3.2



Number of Points: 4498 Sampling Interval: 0.5 hrs

Minimum  $\tau = 0.34298$  s Mean =  $0.34741 s$ Maximum  $\tau = 0.35101$  s Standard Deviation = 0.00117 s

### 40HRLP THERMOCLINE DEPTH RECORDS Fig. 7.2

 $Z_{12}$  Conversion equation:  $Z_{12} = -19000 \text{ms}^{-1} \cdot \tau_d + B$ where  $B = 7365.00 \text{ m}$ Travel Time (sec) with tide removed  $\tau_d =$ 



Number of Points: 365 Sampling Interval: 6.0 hrs



# PIES87B6 (continue)

### MEASURED PRESSURE RECORDS Fig. 4



Number of Points: 4498 Sampling Interval: 0.5 hrs

(Pressure record is jumpy)

### TEMPERATURE RECORDS Fig.  $6$



Number of Points: 4498 Sampling Interval: 0.5 hrs



### 40HRLP TEMPERATURE RECORDS Fig. 9



Number of Points: 363 Sampling Interval: 6.0 hrs



### Table 11. Site and Record Information for **IES87B7**

Serial Number: 036 Type of Travel Time Detector: TTC Number of Pings per Sampling: 20 Additional Sensors: None

POSITION: 35°06.05 N DEPTH: 3800 m 73°31.94 W



### TRAVEL TIME RECORDS Fig. 3.2



Number of Points: 4495 Sampling Interval: 0.5 hrs



### 40HRLP THERMOCLINE DEPTH RECORDS Fig. 7.2

 $Z_{12}$  Conversion equation:  $Z_{12} = -19000 \text{ms}^{-1} \cdot \tau_d + B$ where  $B = 97250.04$  m Travel Time (sec) with tide removed  $\tau_d =$ 



Number of Points: 365 Sampling Interval: 6.0 hrs



### Table 12. Site and Record Information for **IES87C1**

Serial Number: 041 Type of Travel Time Detector: TTC Number of Pings per Sampling: 20 Additional Sensors: None

#### POSITION: 36°02.80 N DEPTH: 2880 m 73°52.90 W



### TRAVEL TIME RECORDS Fig. 3.1



Number of Points: 1489 Sampling Interval: 0.5 hrs

Minimum  $\tau = 3.94585$  s  $Mean = 3.95146 s$ Maximum  $\tau = 3.95906$  s Standard Deviation = 0.00259 s

### 40HRLP THERMOCLINE DEPTH RECORDS Fig. 7.1

 $Z_{12}$  Conversion equation:  $Z_{12} = -19000 \text{ms}^{-1} \cdot \tau_d + B$ where  $B =$ 75455.93 m  $\tau_d =$ Travel Time (sec) with tide removed



Number of Points: 114 Sampling Interval: 6.0 hrs

Minimum  $Z_{12} = 274.26$  m  $Mean = 373.72 m$ Maximum  $Z_{12} = 460.27$  m Standard Deviation = 44.67 m

## Table 13. Site and Record Information for **IES87C2**

Serial Number: 061 Type of Travel Time Detector: TTC Number of Pings per Sampling: 20 Additional Sensors: None

POSITION: 35°43.98 N DEPTH: 3535 m 73°29.98 W



### TRAVEL TIME RECORDS Fig. 3.1



Number of Points: 4622 Sampling Interval: 0.5 hrs



### 40HRLP THERMOCLINE DEPTH RECORDS Fig. 7.1

 $Z_{12}$  Conversion equation:  $Z_{12} = -19000 \text{ms}^{-1} \cdot \tau_d + B$ where  $B = 90375.20 m$  $\tau_d =$  Travel Time (sec) with tide removed



Number of Points: 375 Sampling Interval: 6.0 hrs



#### 3 Half-hourly Data For Each Cross-stream Line

Plots of the travel time records from each instrument are presented first. These are followed by the measured and residual pressure records and the temperature data for the instruments which had those additional sensors.

These are grouped by cross-stream line, with the northwesternmost IES on each line plotted at the top of the figure. Each plot is labelled with the instrument name in the upper left corner. The time scale is the same for all plots, with each increment corresponding to 5 days. The axis begins on 1200 GMT of the first date labelled.

Vertical scale for each variable is consistent between instruments. Each increment corresponds to 5 msec for the travel time records, to 0.5 dbar for the measured bottom pressure measurements, to 0.05 dbar for the residual bottom pressure data, and to 0.1°C for the temperatures.

The sampling interval of the IESs and PIESs is normally 0.5 hours; the actual interval for each instrument is listed Section 2. ATMs have a 6 hour sampling interval. The length and the start and end times of the data records are also listed in the previous section.



Figure 3.1:

Travel time records for Line A and C at half-hourly intervals. The start and end times and records lengths are listed in Section 2.





Figure 3.2: Travel time records for Line B at half-hourly intervals: at sixhourly intervals for ATMs.



B 1986-1987

LINE

PIES87

1966.07



Half-hourly measured bottom pressure records for PIES87B1, PIES87B3 and The start and end times, and records lengths are listed in Section PIES87B6.  $\mathbf{a}$ 

Figure 4:









 $\overline{37}$ 

#### $\overline{4}$ 40 HRLP Data For Each Cross-Stream Line

The low-pass filtered thermocline depth  $(Z_{12})$ , bottom pressure and temperature records are plotted for each cross-stream line. The thermocline depth records for each cross-stream line are presented first. These are followed by the 40 HRLP residual pressure records and the 40 HRLP temperature data for the instruments which had these additional sensors.

The time scale is the same for all plots, with each increment corresponding to 10 days. The axis begins on 1200 GMT of the first date labelled.

Vertical scale for each variable is consistent between instruments. Each increment corresponds to 100 m for the  $Z_{12}$  records, to 0.05 dbar for the bottom pressure measurements, and to 0.1°C for the temperatures. The sampling intervals are 6 hours for all variables of the IESs and PIESs and 24 hours for those of the ATMs. The length and the start and end times of the data records are tabulated in Section 2.



Figure 7.1: Thermocline depth records for Line A and C: records 40HR low-pass filtered at 6 hour intervals. For each instrument, the equation used to convert travel time to  $Z_{12}$  is given in Section  $2.$ 



Figure 7.2: Thermocline depth records for Line B: (P)IESs records 40HR low-pass filtered at 6 hour intervals and ATM records 96HR low-pass filtered at 24 hour intervals.







Figure 9: 40HRLP temperature records for PIES87B1, PIES87B3 and PIES87B6. at 6 hour intervals.

 $\ddot{\phantom{0}}$ 

#### $\overline{5}$ **Thermocline Depth Maps**

 $\lambda$ 

Contour plots of the mean and variance fields and the error fields, the thermocline depth  $(Z_{12})$  fields are presented.

Each of the contoured frames corresponds to the 160 Km by 140 Km boxed region shown in Figure 1. The axes, oriented 045°T, are referenced to a grid origin located at 35°N 75°W. Each frame consists of a  $9 \times 8$  square grid of points, at 20 Km spacing. The actual IES sites are indicated by the  $+$  marks and the positions are listed in Table 1.



field is 25 m with the dashed region corresponding to variance  $\leq$  150 m rms.



Figure 10:



The error bar fields (left) have a contour interval of 10 m and the dashed region corresponds to errors  $<$  50 m. The error (percent variance) fields, shown at right, are contoured at 5% intervals, with the dashed region corresponding to  $<$  15% error. The error maps apply to the  $Z_{12}$  in Figure 12 for the dates shown. Figure 11:

The 12° isotherm depth,  $Z_{12}$ , field is shown at daily intervals from 28 Nov, 1986 to 27 Feb, 1987. The maps are shown for 1200 GMT on the date indicated at the bottom. The Z<sub>12</sub> field is contoured by solid and dashed lines with 100 m intervals. The shorter dashed lines correspond the error maps are shown in Figure 11. Figure 12:





















120.



 $\frac{1}{\sqrt{2}}$ 

 $\mathfrak{z}$ 

### **ACKNOWLEDGMENTS**

The SYNOP Pilot Experiment was supported by the Office of Naval Research under contract number N00014-86-C-0394. We thank the crews of the R/V ENDEAVOR for their efforts during the deployment and recovery cruises. The successful deployment and recovery of the inverted echo sounders is due to the instrument development and careful preparation done by Gerard Chaplin and Michael Mulroney. It is a pleasure to acknowledge their efforts. Special thanks goes to Meghan Cronin and Harris Kontoyiannis who helped in the data processing. Skip Carter supplied the basic objective mapping and contouring programs. The FESTSA time series analysis package was modified for use on the PRIME 750 by David Lai, Eva Griffith, and Mark Wimbush.

### **REFERENCES**

- Brooks, D. A. 1976. (Editor). Fast and Easy Time Series Analysis at NCSU. Technical Report. Center for Marine and Coastal Studies. North Carolina State University. Raleigh, NC.
- Carter, E. F. 1983. The statistics and dynamics of ocean eddies. Ph.D. Thesis. Harvard University.
- Chaplin, G. and D. R. Watts. 1984. Inverted echo sounder development. Oceans '84 Conference Record. 1. 249-253.
- Chaplin, G. and D. R. Watts. 1986. An acoustic ocean-transport meter. IEEE Oceans '86 Proceding, Washington, D.C., Sept, 1986, 426-429
- Dixon, W. J. and M. B. Brown. 1979. (Editor). BMDP 79 Biomedical Computer Programs P-series. University of Caliornia Press. Berkeley, CA. 880 pp
- Munk, W. H. and D. E. Cartwright. 1977. Tidal spectroscopy and prediction. Phios. Trans. R. Soc. London, 259, 533-581.
- Rossby, T. 1969. On monitoring depth variations of the main thermocline acoustically. J. Geophys. Res. 74.5542-5546.
- Tracey, K. L. and D. R. Watts. 1988. Inverted echo sounder processing procedures. University of Rhode Island. GSO Technical Report (in preparation).
- Tracey, K. L., Friedlander, A. I. and D. R. WATTS. 1987. Objective analysis of the Gulf Stream thermal front: method and accuracy. GSO technical Report 87-2.
- Watts, D. R. and W. E. Johns. 1982. Gulf Stream meanders: observations on propagation and growth. J. Geophys. Res. 87. 9467-9476.
- Watts, D. R. and H. Kontoyiannis. 1986. Deep-ocean bottom pressure and temperature sensors report: methods and data. University of Rhode Island. GSO Technical Report 86-8. 111 pp.
- Watts, D. R. and H. T. Rossby. 1977. Measuring dynamic heights with inverted echo sounders: Results from MODE. J. Phys. Oceanogr. 7. 345-358.
- Watts, D. R., K. L. Tracey and A. I. Friedlander. 1988. Processing accurate maps of the Gulf Stream thermal front using objective analysis. J. Geophys. Res. (submitted)
- Watts, D. R. and M. Wimbush. 1981. Sea surface height and thermocline depth variations measured from the sea floor. International Symposium on Acoustic Remote Sensing of the Atmosphere and Oceans, Proceedings, Calgary, Alberta, Canada.



 $\cdot$ 

 $\mathcal{O}(\mathcal{F}^{\mathcal{O}}_{\mathcal{O}})$  and

 $\mathcal{A}$ 

 $\mathcal{L}^{\mathcal{A}}$ 

 $\bullet$ 

 $\mathcal{A}^{\mathcal{A}}$ 

 $\ddot{\phantom{0}}$ 

 $\frac{1}{\sqrt{2}}$ 

 $\ddot{\phantom{a}}$ 

Current Meters, Acoustic Transport Meters

 $\ddot{\mathcal{L}}$  .

j.

÷,